Results of Proficiency Test Liquefied Propane & Sulfur (total) in LPG October 2020

Organized by: Institute for Interlaboratory Studies

Spijkenisse, the Netherlands

Author: ing. G.A. Oosterlaken-Buijs

Correctors: ing. A.S. Noordman-de Neef & ing. R.J. Starink

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CONTENTS

1	INTRODUCTION	3
2	SET UP	3
2.1	QUALITY SYSTEM	3
2.2	PROTOCOL	4
2.3	CONFIDENTIALITY STATEMENT	4
2.4	SAMPLES	4
2.5	STABILITY OF THE SAMPLES	5
2.6	ANALYZES	5
3	RESULTS	6
3.1	STATISTICS	6
3.2	GRAPHICS	7
3.3	Z-SCORES	7
4	EVALUATION	8
4.1	EVALUATION PER SAMPLE AND PER TEST	8
4.2	PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES	12
4.3	COMPARISON OF THE PROFICIENCY TEST OF OCTOBER 2020 WITH PREVIOUS PTS	13
5	DISCUSSION	14

Appendices:

1.	Data, statistical and graphic results	16
2.	Number of participants per country	45
3	Abbreviations and literature	16

1 Introduction

Since 2009 the Institute for Interlaboratory Studies (iis) organizes a proficiency scheme for the analysis of Liquefied Propane every year. From 2017 onwards a proficiency scheme for the analysis of Sulfur (total) in LPG is organized every year as well. During the annual proficiency testing program 2020/2021 it was decided to continue the round robin for both the analysis of Liquefied Propane and for the analysis of Sulfur (total) in LPG.

Because iis has limited gas-handling facilities in place to prepare gas samples, a cooperation with EffecTech (Uttoxeter, United Kingdom) was set up for the Liquefied Propane PT (iis20S03P) and a co-operation with Nippon Gases (Belgium) was set up for the Sulfur (total) in LPG PT (iis20S03S). Both EffecTech and Nippon Gases are fully equipped and have experience in the preparation of gas mixtures.

In the interlaboratory studies for Liquefied Propane 47 laboratories in 28 different countries and for Sulfur (total) in LPG 33 laboratories in 20 different countries registered for participation. In this report, the results of the proficiency tests Liquefied Propane and Sulfur (total) in LPG are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT). In this proficiency test, the participants received, depending on the registration, one or two samples, see table below.

PT	Sample ID	Sample	Size	Purpose
iis20S03P	#20200	Liquefied Propane mixture	one cylinder of 1L	Composition and Physical properties
iis20S03S	#20201	LPG mixture with DMS	one cylinder of 5L	Total Sulfur

Table 1: samples used in Liquefied Propane PT and in Sulfur (total) in LPG PT

The limited cylinder sizes (1L and 5L) are chosen to optimize sample stability, cylinder costs, transport and handling costs.

Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 QUALITY SYSTEM

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, has implemented a quality system based on ISO/IEC17043:2010. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

EffecTech is accredited in conformance with ISO/IEC17043:2010 by UKAS (no. 4719) and ISO17025:2005 by UKAS (no. 0590). Nippon Gases is accredited in conformance with ISO 9001:2015 and ISO 14001.

2.2 PROTOCOL

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

For the liquefied Propane mixture it was decided to prepare a uniquely coded 1L cylinder to optimize the costs for the participants. The mixture was divided over a batch of 56 cylinders (with dip tube device) and tested for homogeneity by EffecTech (Uttoxeter, United Kingdom) in conformance with ISO guide 35:2006 and ISO17025:2017 (job 20/0953). Each cylinder was filled with approximately 200 grams of Liquefied Propane mixture and labelled #20200. Every cylinder in the batch was analyzed using replicate measurements. The within bottle and between bottle variations were assessed in accordance with ISO Guide 35:2006. This evaluation showed that all between bottle variations were small compared to the uncertainties on the reference values on each component.

The repeatability values (r) were calculated per component by multiplication of the respective standard deviation by 2.8. Subsequently, the calculated repeatabilities were compared with 0.3 times the corresponding reproducibility of the reference method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	r (observed) in %mol/mol	0.3 * R (D2163:14(2019)) in %mol/mol
Ethane	0.0009	0.0341
Propane	0.0223	1.2380
Propene	0.0038	0.0733
iso-Butane	0.0104	0.0756
n-Butane	0.0087	0.0648
1-Butene	0.0009	0.0199
iso-Butene	0.0009	0.0236
n-Pentane	0.0039	0.0268

Table 2: homogeneity test results of subsamples #20200

The calculated repeatabilities were in agreement with 0.3 times the corresponding reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the Sulfur (total) in LPG sample a batch of 34 uniquely coded 5L cylinders (with dip tube device) was prepared and tested for homogeneity by Nippon Gases (Belgium) in conformance with ISO9001 and ISO14001 (ref. nr. 416.059.001; order nr. 308578 – Total Sulphur). Each cylinder was filled with approximately 1500 grams of LPG and spiked with Dimethyl Sulfide (DMS) and labelled #20201.

The repeatability of the determination of Total Sulfur for all cylinders were calculated by multiplication of the deviation by 2.8. Subsequently, the calculated repeatability was compared with 0.3 times the corresponding reproducibility of the reference method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Total Sulfur in mg/kg
r (observed)	2.1
reference test method	ASTM D6667:14(2019)
0.3 * R (ref. test method)	3.2

Table 3: evaluation of the repeatability of subsamples #20201

The calculated repeatability was in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

Depending on the registration to each of the participating laboratories 1 cylinder of Liquefied Propane labelled #20200 and/or 1 cylinder with Sulfur in LPG labelled #20201 was sent on September 23, 2020. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

EffecTech (Uttoxeter, United Kingdom) and Nippon Gases (Belgium) declare that the prepared gas cylinders have a shelf life of at least 6 months. This is sufficient for the proficiency testing purposes.

2.6 ANALYZES

The participants were requested to determine on sample #20200: Ethane, Propane, Propene, iso-Butane, n-Butane, 1-Butene, iso-Butene, n-Pentane, iso-Pentane, Molar Mass, Relative Density at 60/60°F, Absolute and Relative Vapor pressure at 100°F, Absolute and Relative Vapor pressure at 40°C, Motor Octane Number (MON), Ideal Gross Heating Value and Ideal Net Heating Value at 14.696 psia and 60°F.

The participants were requested to determine on sample #20201: Total Sulfur.

It was explicitly requested to treat the sample as if it was a routine sample and to report the test results using the indicated units on the report form and not to round the test results, but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods (when applicable) that will be used during the evaluation. The detailed report form

and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyzes). Additional or corrected test results are used for data analysis and the original test results are placed under 'Remarks' in the result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the results of the statistical evaluation should be used with due care.

According to ISO5725 the original test results per determination were submitted to Dixon's, Grubbs' or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by D(0.05) for the Grubbs' test and by D(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement

based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1. was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis.

The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve was projected over the Kernel Density Graph for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM, ISO or EN reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used, like Horwitz or an estimated reproducibility based on former iis proficiency tests.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

 $z_{\text{(target)}} = \text{(test result - average of PT)} / \text{target standard deviation}$

The $z_{\text{(target)}}$ scores are listed in the test result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. Therefore, the usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

4 **EVALUATION**

In this interlaboratory study some problems were encountered with the dispatch of the samples due to the COVID-19 pandemic. Therefore, the reporting time on the data entry portal was extended with another week.

For the Liquefied Propane PT (iis20S03P) four participants reported after the extended reporting date and four participants did not report any test results. Not all participants were able to report test results for all requested tests.

In total 43 participants reported 550 numerical test results. Observed were 35 outlying test results, which is 6.4%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

For the Sulfur in LPG PT (iis20S03S) three participants reported after the extended reporting date and five participants did not report any test results. In total 28 participants reported 28 numerical test results. Observed were 4 outlying test results, which is 14.3%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

Not all original data sets proved to have normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

4.1 EVALUATION PER SAMPLE AND PER TEST

In this section the reported test results are discussed per sample and per test. The test methods which were used by the various laboratories were taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the original data. The abbreviations, used in these tables, are explained in appendix 3.

In the iis PT reports, ASTM methods are referred to with a number (e.g. D2163) and an added designation for the year that the method was adopted or revised (e.g. D2163:14). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D2163:14(2019)). In the test results tables of appendix 1 only the method number and year of adoption or revision (e.g. D2163:14) will be used.

Because the majority of the participating laboratories used ASTM D2163 as test method for the determination of the Propane Composition, it was decided to use the reproducibilities of this test method as target reproducibilities, and to mention the reproducibilities of EN27941 (identical to IP405 and ISO7941) for reference only. In ASTM D2163 no reproducibilities of 1-Butene and iso-Butene are mentioned, the reproducibilities of n-Butane were used to calculate the reproducibilities of these two components.

Three laboratories (495, 1135 and 6203) reported deviating test results for many of the gas composition test results. At least four of the nine test results were statistical outliers. As the nine test results are not independent it was decided not to use any of the reported results of these laboratories for the statistical evaluation. This means that the remaining reported test results were excluded. Also, the reported test results for the parameters calculated from the measured Gas Composition were excluded for these laboratories.

Furthermore, two other laboratories (1011 and 6193) had a large deviation for the sum of the composition results. Since the composition was not normalized the calculated parameters were excluded for the statistical evaluation, when not marked as a statistical outlier.

sample #20200

Ethane:

The determination of this component was not problematic. One statistical outlier was observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14(2019) and in agreement with the reproducibility requirements of EN27941:93(liq).

Propane:

The determination of this component was not problematic. Two statistical outliers were observed and one other test result was excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14(2019) but is not in agreement with the reproducibility requirements of EN27941:93(liq).

Propene:

The determination of this component was not problematic. Two statistical outliers were observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14(2019) and in agreement with the reproducibility requirements of EN27941:93(liq).

iso-Butane:

The determination of this component was problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D2163:14(2019) and is not in agreement with the reproducibility requirements of EN27941:93(liq).

n-Butane:

The determination of this component was problematic. Six statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D2163:14(2019) but is in agreement with the reproducibility requirements of EN27941:93(liq).

1-Butene:

The determination of this component was not problematic. Two statistical outliers were observed and one other test results was excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14(2019) and in agreement with the reproducibility requirements of EN27941:93(liq).

iso-Butene:

The determination of this component was not problematic. Four statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14(2019) and in agreement with the reproducibility requirements of EN27941:93(liq).

n-Pentane:

The determination of this component was very problematic. Six statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not at all in agreement with the requirements of ASTM D2163:14e1(2019). Therefore, it was decided to calculate no z-scores. The calculated reproducibility after rejection of the statistical outliers is in agreement with the reproducibility requirements of EN27941:93(liq).

iso-Pentane:

The determination of this component may not be problematic. Most of the laboratories agreed that the amount of iso-Pentane was lower than 0.01 %mol/mol, therefore no z-scores were calculated.

Total of the composition results: The sum of the test results of the composition per laboratory was calculated by iis. Since the composition results are requested as normalized, every laboratory should have an outcome of 100%. Two calculated results were found to be significantly different than 100. It was decided to exclude these test results in the evaluations of the Physical Properties.

Molar Mass:

This calculated parameter may not be problematic. One statistical outlier was observed and three other test results were excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published molar mass factors obtained from ASTM D2421:19 over all reported component concentrations (0.18 vs. 0.17 g/mol).

Rel. Density at 60°F: This calculated parameter may not be problematic. Two statistical outliers were observed and three other test result were excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published relative density factors obtained from ASTM D2598:16 over all reported component concentrations (0.0012 vs. 0.0010).

<u>Abs. VP at 100°F</u>: As the reported results calculated via ISO8973 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

ISO8973; This calculated parameter may be problematic. One statistical outlier was observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (3.08 vs. 1.40 psi).

ASTM D2598; This calculated parameter may be problematic. No statistical outliers were observed but one test result was excluded. The calculated reproducibility after rejection of the suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from ASTM D2598:16 over all reported component concentrations (3.53 vs. 1.73 psi).

Rel. VP at 100°F: As the reported results calculated via ISO8973 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

ISO8973; This calculated parameter may not be problematic. One statistical outlier was observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (1.03 vs. 1.40 psi).

ASTM D2598; This calculated parameter may be problematic. One statistical outlier was observed and one other test result was excluded. The calculated reproducibility after rejection of the suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from ASTM D2598:16 over all reported component concentrations (2.89 vs. 1.73 psi).

- <u>Abs. VP at 40°C</u>: This determination may be problematic. No statistical outliers were observed but four test results were excluded. The calculated reproducibility after rejection of the suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (18.2 vs. 9.9 kPa).
- Rel. VP at 40°C: This determination may be problematic. One statistical outlier was observed and four other test results were excluded. The calculated reproducibility after rejection of the suspect data is larger than with the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (12.8 vs. 9.9 kPa).

MON: As the reported results calculated via EN589 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

EN589; This calculated parameter may be problematic. Three statistical outliers were observed and three other test results were excluded. The calculated reproducibility after rejection of suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from EN589:18 over all reported component concentrations (0.33 vs. 0.07).

D2598; Due to the low number of reported test results it was decided to drawn no conclusions.

Ideal Gross Heating Value at 14.696 psia / 60°F: In this PT none of the participants reported to have used ISO6976, therefore the results for all laboratories were only calculated according to ASTM D3588.

This calculated parameter may be problematic. No statistical outlier was observed but one test result was excluded. The calculated reproducibility after rejection of the suspect data is in larger than the calculated reproducibility using the published Ideal Gross Heating Values obtained from EN3588:98(2017) over all reported component concentrations (12 vs. 8).

Ideal Net Heating Value at 14.696 psia / 60°F: In this PT none of the participants reported to have used ISO6976, therefore the results for all laboratories were only calculated according to ASTM D3588.

This calculated parameter may be problematic. No statistical outlier was observed but one test result was excluded. The calculated reproducibility after rejection of the suspect data is in larger than the calculated reproducibility using the published Ideal Gross Heating Values obtained from EN3588:98(2017) over all reported component concentrations (12 vs. 7).

sample #20201

Total Sulfur:

The determination of this component was problematic. Four statistical outliers were observed. The calculated reproducibility after rejection of the outliers is not in agreement with the requirements of ASTM D6667:14(2019).

4.2 Performance evaluation for the group of Laboratories

A comparison has been made between the reproducibility as declared by the reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from literature reference test methods (in casu ASTM D2163) or based on previous proficiency tests are presented in the next table.

Component	unit	n	average	2.8 * sd	R(D2163)	R(EN27941) liqinj.
Ethane	%mol/mol	39	0.194	0.057	0.111	0.301
Propane	%mol/mol	40	91.84	1.28	4.12	1.02
Propene	%mol/mol	39	0.779	0.106	0.241	0.215
iso-Butane	%mol/mol	40	2.926	0.465	0.254	0.389
n-Butane	%mol/mol	37	2.817	0.370	0.219	0.389
1-Butene	%mol/mol	40	0.203	0.034	0.067	0.161
iso-Butene	%mol/mol	39	0.289	0.055	0.079	0.161
n-Pentane	%mol/mol	37	0.939	0.321	(0.091)*	(0.313)*
iso-Pentane	%mol/mol	27	<0.01	n.e.	n.e.	n.e.

Table 4: reproducibilities of the composition of sample #20200

^{*)} results in brackets should be used with due care

Parameter	unit	n	average	2.8 * sd	R(all calc.)*
Molar Mass	g/mol	21	45.19	0.18	0.17
Rel. Density at 60/60°F		22	0.5135	0.0012	0.0010
Abs. VP at 100°F ISO/IP	psi	8	183.2	3.1	1.4
Abs. VP at 100°F D2598	psi	7	179.6	3.5	1.7
Rel. VP at 100°F ISO/IP	psi	8	168.1	1.0	1.4
Rel. VP at 100°F D2598	psi	12	164.4	2.9	1.7
Abs. VP at 40°C	kPa	20	1295	18	10
Rel. VP at 40°C	kPa	19	1193	13	10
MON EN589		11	95.05	0.33	0.07
MON D2598		5	96.24	(0.62)**	0.09
IGHV D3588	kJ/mol	11	2269	12	8
INHV D3588	kJ/mol	11	2088	12	7

Table 5: reproducibilities of calculated parameters on sample #20200 using one set of factors.

Component	unit	n	average	2.8 * sd	R(lit)
Total Sulfur	mg/kg	24	31.8	13.6	9.9

Table 6: reproducibility of test on sample #20201

Without further statistical calculations it can be concluded that for several components there is not a good compliance of the group of participating laboratories with the relevant reference test method. The problematic components have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF OCTOBER 2020 WITH PREVIOUS PTs

	October 2020	October 2019	October 2018	October 2017	October 2016
Number of reporting laboratories	43	46	44	47	43
Number of test results	550	574	495	536	472
Number of statistical outliers	35	48	20	30	34
Percentage of statistical outliers	6.4%	8.4%	4.0%	5.6%	7.2%

Table 7: comparison with previous proficiency tests on Liquefied Propane (excluded Sulfur in LPG)

	October 2020	October 2019	October 2018	October 2017
Number of reporting laboratories	28	13	15	8
Number of test results	28	13	15	8
Number of statistical outliers	4	0	1	1
Percentage of statistical outliers	14.3%	0%	6.7%	12.5%

Table 8: comparison with previous proficiency tests on Sulfur in LPG only

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the reference test methods. The conclusions are given the following tables.

^{*)} calculation based on all reported composition results
**) results in brackets should be used with due care

Component	October 2020	October 2019	October 2018	October 2017	October 2016
Ethane	+	+	++	++	++
Propane	++	++	++	++	++
Propene	++	++	++	++	++
iso-Butane	-	+	-	+/-	-
n-Butane	-	+/-		-	-
1-Butene		++	+	++	++
iso-Butene	-	+	+	++	+
n-Pentane	()	+/-	-	-	-
iso-Pentane	n.e.	n.a.	n.a.	n.a.	n.a.

Table 9: comparison determinations on Liquefied Propane against the reference test methods

^{**)} results in brackets should be used with due care

Component	October	October	October	October
	2020	2019	2018	2017
Total Sulfur	-	+	-	+

Table 10: comparison determinations on Sulfur in LPG against the reference test method

The following performance categories were used:

- ++: group performed much better than the reference test method
- + : group performed better than the reference test method
- +/-: group performance equals the reference test method
- : group performed worse than the reference test method
- -- : group performed much worse than the reference test method
- n.e.: not evaluated

5 DISCUSSION

The consensus values as determined in this PT are compared with the average values from the homogeneity testing by EffecTech (Uttoxeter, United Kingdom) in the following table. From this comparison it is clear that most consensus values as determined in this PT are very well in line with the values as determined during the preparation of the gas cylinders.

Parameter	Average by EffecTech in %mol/mol	Average from participants in %mol/mol	Difference in %mol/mol	z-score
Ethane	0.201	0.194	0.194 0.007	
Propane	92.005	91.843	0.162	0.11
Propene	0.792	0.778	0.014	0.16
iso-Butane	2.884	2.926	-0.042	-0.46
n-Butane	2.727	2.817	-0.090	-1.15
1-Butene	0.198	0.203	-0.005	-0.19
iso-Butene	0.288	0.289	-0.001	-0.02
n-Pentane	0.904	0.939	-0.034	(-1.06)*

Table 11: comparison of consensus values with values determined by EffecTech

^{*)} results in brackets should be used with due care

In principle no additional variation should be introduced when applying a calculation on the reported component concentrations. However, in practice a significant additional uncertainty is added in most cases. See the differences between the values from the test results as reported by the participating laboratories (each using its own calculation procedure) and the values as calculated by its using one calculation procedure for each set of laboratory test results (see table 5).

Different test methods for the calculation of the Vapor Pressure do exist. Specification EN589 refers to ISO8973 for the calculation of Vapor Pressure. In ISO8973 (identical to IP432) the Vapor Pressure is calculated from the <u>mole fraction</u> per component and a Vapor Pressure factor of that component (given for all components). In ASTM D2598 the Vapor Pressure is calculated from the <u>liquid volume percentage</u> per component and a Vapor Pressure factor of that component (given for only some components).

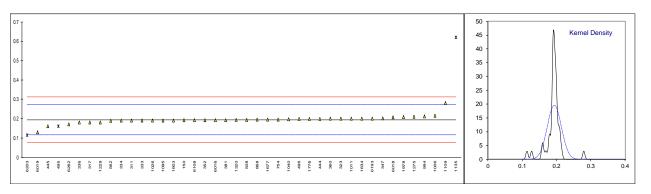
For the MON, the calculation in Annex B from specification EN589 is used by iis on a molar basis, while ASTM D2598 describes the calculation of MON on a liquid volume basis. Also, the selection of the tables for the component factors to be used for the calculations may cause additional uncertainty.

It is remarkable to see that the results for Vapor Pressure from the ASTM D2598 calculation are significantly lower than the results from the ISO8973/IP432 calculation. The observed difference is caused by a difference in the VP factor of Ethane. ASTM (Subcommittee D02.H) commented (see also lit. 14):

"The vapor pressure of ethane in D2598 was revised a few times prior to 2002. The current value, 611 psi, has remained the same for the last ten years. The revision of ethane was done because components in LPG blends do not necessarily behave as ideal gases. In particular, properties of ethane and ethylene appear to differ from ideality. Factors for these two components have been modified from 'ideal gas' values to make the calculated vapor pressure results more closely approximate actual measured vapor pressures of LPG blends. (i.e. D1267). Chapter 2 of Fuels and Lubricants Handbook (George Totten, © 2003), states that calculated vapor pressure were found to be biased high relative to experimental vapor pressure measured by D1267 for high ethane samples in earlier versions of D2598'.

APPENDIX 1
Determination of Ethane on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	0.191	IIIai K	-0.08	Telliaiks
171	DZ 103	0.191		-0.06	
311	D2163	0.19		-0.10	
317	D2163	0.18		-0.16	
323	D2163	0.20		0.15	
333	D2163	0.19		-0.10	
334	D2163	0.19		-0.10	
335	D2163	< 0.01		<-4.65	possibly a false negative test result?
336	D2163	0.18		-0.36	possibly a raise negative test result:
347	D2163	0.201		0.17	
352	EN27941	0.1914		-0.07	
360	EN27941	0.20		0.15	
381	DIN51619	0.192		-0.05	
444	IP405	0.198		0.10	
445	D2163	0.16		-0.86	
495	D2163	0.16	ex	-0.86	test result excluded, see §4.1
496	D2163	0.197	O.A.	0.07	toot room oxoradou, ooo 3
508	D2163	0.193056		-0.03	
529	22.00				
562	D2163	0.188		-0.15	
754	D2163	0.195		0.02	
868	D2163	0.194		0.00	
994	D2163	0.2102		0.41	
1006	D2163	0.215		0.53	
1011	ISO7941	0.2		0.15	
1026	ISO7941	0.19	С	-0.10	first reported 0.23
1040	DIN51619Mod.	0.196		0.05	
1095	ISO7941	0.19		-0.10	
1109	IP405	0.28		2.17	
1135	D2163	0.62	R(0.01)	10.75	
1229	IP473	0.18	, ,	-0.36	
1275	EN27941	0.209		0.38	
1320	D2163	0.193		-0.03	
1469					
1603		0.1900		-0.10	
1634	ISO7941	0.20		0.15	
1677		0.194		0.00	
1776	EN27941	0.197	С	0.07	first reported 0.654
1978	D2163	0.2080		0.35	
6016	GOST10679	0.1918		-0.06	
6018	EN27941	0.2067		0.32	
6019	ISO7941	0.1281		-1.67	
6108	D2163	0.1911		-0.08	
6142					
6193	D2163	0.20		0.15	
6203	EN27941	0.1144	ex	-2.01	test result excluded, see §4.1
6262	D2163	0.1696		-0.62	
	normality	not OK			
	n	39			
	outliers	1 (+2 ex)			
	mean (n)	0.1941			
	st.dev. (n)	0.02039			
	R(calc.)	0.0571			
	st.dev.(D2163:14)	0.03962			
	R(D2163:14)	0.1109			Compare R(EN27941:13(liq)) = 0.3005

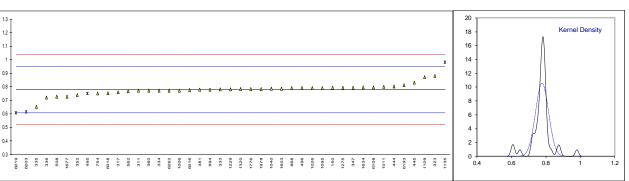


Determination of Propane on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	92.132		0.20	
171	D2100				
311	D2163	91.84		0.00	
317	D2163	91.86		0.01	
323	D2163	90.97		-0.59	
333	D2163	91.74		-0.07	
334	D2163	91.82		-0.07	
335					
	D2163	91.71		-0.09	
336	D2163	92.27		0.29	
347	D2163	92.449		0.41	
352	EN27941	91.5927		-0.17	
360	EN27941	91.96		80.0	
381	DIN51619	91.82		-0.02	
444	IP405	91.521		-0.22	
445	D2163	91.71		-0.09	test models and old a sec CAA
495	D2163	89.71	ex	-1.45	test result excluded, see §4.1
496	D2163	91.631		-0.14	
508	D2163	90.450463		-0.95	
529					
562	D2163	91.728		-0.08	
754	D2163	92.489		0.44	
868	D2163	91.719		-0.08	
994	D2163	91.8071		-0.02	
1006	D2163	92.146		0.21	
1011	ISO7941	92.6		0.51	
1026	ISO7941	91.51	С	-0.23	first reported 93.99
1040	DIN51619Mod.	92.245		0.27	
1095	ISO7941	91.69		-0.10	
1109	IP405	92.93		0.74	
1135	D2163	95.74	R(0.01)	2.65	
1229	IP473	91.79		-0.04	
1275	EN27941	91.895		0.04	
1320	D2163	91.806		-0.03	
1469					
1603		91.5209		-0.22	
1634	ISO7941	91.19		-0.44	
1677		91.984		0.10	
1776	EN27941	91.82	С	-0.02	first reported 95.803
1978	D2163	92.3483	•	0.34	
6016	GOST10679	91.7166		-0.09	
6018	EN27941	92.4913		0.44	
6019	ISO7941	91.8362		0.00	
6108	D2163	91.7472		-0.07	
6142	22.00				
6193	D2163	91.06		-0.53	
6203	EN27941	84.4891	R(0.01)	-5.00	
6262	D2163	92.1746	11(0.01)	0.23	
0202	D2100	02.17 1 0		0.20	
	normality	suspect			
	n	40			
	outliers	2 (+1 ex)			
	mean (n)	91.8430			
	st.dev. (n)	0.45791			
	R(calc.)	1.2821			
	st.dev.(D2163:14)	1.47197			
	R(D2163:14)	4.1215			Compare R(EN27941:13(liq)) = 1.0245
	N(D2103.14)	4.1213			Compare $N(LN27941.13(IIq)) = 1.0243$
100 T					1.4
98 -					1.2 - Kernel Density
96					x
94 -					1 -
92		<u> </u>		<u> </u>	
90 x A					0.8 -
88 - X					0.6 -
86 +					0.4
84 X					0.2
1 82 ↓					I 0.2]

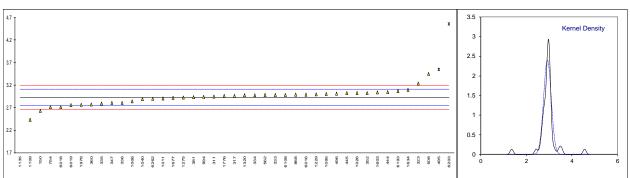
Determination of Propene on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	0.791		0.15	
171	_				
311	D2163	0.77		-0.10	
317	D2163	0.76		-0.21	
323	D2163	0.88		1.18	
333	D2163	0.78		0.02	
334	D2163	0.77		-0.10	
335	D2163	0.65		-1.49	
336 347	D2163 D2163	0.72 0.793		-0.68 0.17	
352	EN27941	0.7382		-0.47	
360	EN27941	0.7362		-0.47	
381	DIN51619	0.777		-0.10	
444	IP405	0.802		0.02	
445	D2163	0.83		0.60	
495	D2163	0.75	ex	-0.33	test result excluded, see §4.1
496	D2163	0.789		0.12	3 ···
508	D2163	0.725490		-0.61	
529					
562	D2163	0.765		-0.16	
754	D2163	0.750		-0.33	
868	D2163	0.789		0.12	
994	D2163	0.7774		-0.01	
1006	D2163	0.771		-0.09	
1011	ISO7941	8.0		0.25	
1026	ISO7941	0.79	С	0.13	first reported 0.81
1040	DIN51619Mod.	0.785		0.08	
1095	ISO7941	0.79		0.13	
1109	IP405	0.87	0(0.04)	1.06	
1135	D2163	0.98	G(0.01)	2.34	
1229 1275	IP473 EN27941	0.78 0.791		0.02 0.15	
1320	D2163	0.791		0.13	
1469	D2103	0.762			
1603		0.7853		0.08	
1634	ISO7941	0.795		0.19	
1677		0.727		-0.60	
1776	EN27941	0.782	С	0.04	first reported 0.994
1978	D2163	0.7820		0.04	
6016	GOST10679	0.7753		-0.04	
6018	EN27941	0.7519		-0.31	
6019	ISO7941	0.6052	G(0.05)	-2.01	
6108	D2163	0.7953		0.20	
6142	_				
6193	D2163	0.81		0.37	
6203	EN27941	0.6140	ex	-1.91	test result excluded, see §4.1
6262	D2163	0.7706		-0.09	
		. 014			
	normality	not OK			
	n 	39			
	outliers	2 (+2 ex)			
	mean (n)	0.7785			
	st.dev. (n) R(calc.)	0.03785 0.1060			
	st.dev.(D2163:14)	0.1000			
	R(D2163:14)	0.2413			Compare R(EN27941:13(liq)) = 0.2147
	,				



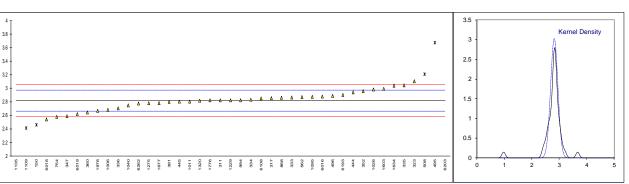
Determination of iso-Butane on sample #20200; results in %mol/mol

150 D2163	lab	method	value	mark	z(targ)	remarks
311 D2163		D2163	2.626		-3.31	
323 D2163						
323 D2163 3.23 3.36 3.38 3.36 3.33 3.36 3.33 D2163 2.98 0.60 3.34 D2163 2.97 0.49 3.35 D2163 2.79 1.50 3.36 D2163 2.80 1.39 3.37 D2163 2.80 1.40 3.52 EN27941 3.0227 1.07 3.52 EN27941 3.0227 1.07 3.52 EN27941 3.0227 1.07 3.52 EN27941 3.022 1.04 4.54 D2163 3.02 1.04 4.55 D2163 3.02 1.04 4.55 D2163 3.02 1.04 4.55 D2163 3.04 7776 5.77 5.79 5.09 5.00 EN2763 2.935 0.66 6.79 5.00 EN2763 2.935 0.66 6.79 5.77 5.29 5.29 5.20 5.20 5.20 5.20 5.20 5.20 5.20 5.20						
333 D2163						
334 D2163					3.36	
336 D2163						
336 D2163						
347 D2163						
352 ENZ7941 3.0227 1.07 360 ENZ7941 2.277 -1.72 381 DIN51619 2.297 0.02 444 IP405 3.042 1.29 445 D2163 3.02 1.04 445 D2163 3.02 1.04 446 D2163 3.04 R(0.05) 6.79 496 D2163 3.04 R(0.05) 6.79 508 D2163 3.447776 5.77						
360 ENZ7941 2.77 -1.72 381 DIN51619 2.927 0.02 444 IP405 3.042 1.29 445 D2163 3.54 R(0.05) 6.79 496 D2163 3.54 R(0.05) 6.79 496 D2163 3.004 0.87 508 D2163 3.447776 5.77 509 500 D2163 2.975 0.55 754 D2163 2.975 0.55 754 D2163 2.985 0.66 D2163 2.985 0.66 D2163 2.886 -0.99 1011 IS07041 2.9 -0.28 1026 IS07041 3.02 C 1.04 1040 DIN51619Mod. 2.889 -0.40 1050 ISC7941 3.00 0.62 1109 IP405 2.43 R(0.01) 17.29 1209 IP473 2.99 0.71 1320 D2163 2.968 0.47 1330 D2163 2.981 0.71 1340 DIN51619Mod. 2.989 0.71 1350 D2163 2.985 0.06 6018 ISO7941 3.09 1.82 1677 2.914 0.13 1684 ISO7941 2.99 0.71 1776 ENZ7941 2.995 0.01 1804 ISO7941 3.09 1.82 1677 2.914 0.13 1684 ISO7941 2.985 0.06 6018 ISO7941 2.985 0.66 6018 ENZ7941 2.985 0.66 6018 ENZ7941 2.7605 -1.92 6016 GOST10679 2.9853 0.66 6018 ENZ7941 2.7605 -1.93 6018 GST0941 2.7605 -1.93 6019 ISO7941 2.7509 1.93 6018 GST10679 2.9853 0.66 6018 ENZ7941 2.7605 -1.93 6019 ISO7941 2.7509 1.93 6019 ISO7941 2.7509 1.93 6019 ISO7941 2.7509 1.93 6019 ISO7941 2.7509 1.93 6020 ENZ7941 2.7605 -1.93 6030 ENZ7941 2.7605 1.93 6030 ENZ7941 2.9						
381 DINS1619 2.927 0.02 444 IP405 3.042 1.29 445 D2163 3.02 1.04 485 D2163 3.04 R(0.05) 6.79 486 D2163 3.04 R(0.05) 6.79 508 D2163 3.447776 5.77 529 562 D2163 2.975 0.55 754 D2163 2.975 0.55 754 D2163 2.935 0.66 80 D2163 2.9391 0.15 1006 D2163 2.836 -0.99 1011 ISC7941 2.9 C 1.04 first reported 2.23 1040 DINS1619Mod. 2.889 -0.40 1095 ISC7941 3.00 0.82 1109 IP405 2.43 1.36 R(0.01) 1.729 1229 IP473 2.99 0.71 1275 ENZ7941 2.925 -0.01 1230 D2163 2.986 0.47 1469					1.07	
444 P405 3.042 1.29 445 D2163 3.54 R(0.05) 6.79 496 D2163 3.047776 5.77 529					1.72	
445 D2163 3.02 1.04 495 D2163 3.04 R(0.05) 6.79 496 D2163 3.04 R(0.05) 6.79 508 D2163 3.44776 5.77 529						
495 D2163						
486 D2163				R(0.05)		
508 D2163				11(0.00)		
529 529 520 52163 52975 520 52163 52975 520 52163 52985 529 52163 52985 529 52163 52985 529 52163 52985 529 52163 52985 529 52163 52985 529 52163 52985 529 52163 52981 529 52163 52981 529 529 529 529 529 529 529 529 529 529						
754 D2163						
888 D2163	562	D2163	2.975		0.55	
994 D2163	754	D2163	2.707		-2.41	
1006 D2163	868	D2163	2.985		0.66	
1011 ISO7941 2.9 -0.28 1026 ISO7941 3.02 C 1.04 first reported 2.23 1040 DIN51619Mod. 2.889 -0.40 1095 ISO7941 3.00 0.82 1109 IP405 2.43 -5.47 1135 D2163 1.36 R(0.01) -17.29 1229 IP473 2.99 0.71 1375 ENZ7941 2.925 -0.01 1320 D2163 2.968 0.47 1469 1634 ISO7941 3.09 1.82 1677 2.914 -0.13 1776 ENZ7941 2.955 C 0.33 first reported 1.300 1978 D2163 2.7605 -1.82 6016 GOST10679 2.9853 0.66 6018 ENZ7941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6018 ENZ7941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6108 D2163 2.9815 0.62 61142 6193 D2163 3.06 1.49 6203 ENZ7941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 R(calc.) 0.4647 st.dev. (D) 0.16595 R(calc.) 0.4647 st.dev. (D) 0.9053 R(D2163:14) 0.90903 R(D2163:14) 0.90903 R(D2163:14) 0.90903 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
1026 ISO7941 3.02 C 1.04 first reported 2.23 1040 DIN51619Mod. 2.889 -0.40 1095 ISO7941 3.00 0.82 1109 IP405 2.43 -5.47 1135 D2163 1.36 R(0.01) -17.29 1229 IP473 2.99 0.71 1275 EN27941 2.925 -0.01 1320 D2163 2.968 0.47 1469						
1040 DINS1619Mod. 2.889 -0.40 1095 ISO7941 3.00 0.82 1109 IP405 2.43 -5.47 1135 D2163 1.36 R(0.01) -17.29 1229 IP473 2.99 0.71 1275 EN27941 2.925 -0.01 1320 D2163 2.968 0.47 1634 ISO7941 3.09 1.82 1667 2.914 -0.13 1776 EN27941 2.955 C 0.33 first reported 1.300 1978 D2163 2.7605 -1.82 6016 GOST10679 2.9853 0.66 6018 EN27941 2.7083 -2.40 6019 ISO7941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142				_		
1095 SO7941 3.00 0.82 1109 P405 2.43 -5.47 1135 D2163 1.36 R(0.01) -17.29 1229 P473 2.99 0.71 1275 EN27941 2.925 -0.01 1320 D2163 2.968 0.47 1469 1603 3.0316 1.17 1634 ISO7941 3.09 1.82 1677 2.914 -0.13 1676 EN27941 2.955 C 0.33 1677 2.955 C 0.33 1978 D2163 2.7605 -1.82 6016 GOST10679 2.9853 0.66 6018 EN27941 2.7509 -1.93 6018 EN27941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n				С		first reported 2.23
1135 D2163						
1229 IP473 2.99 0.71 1275 EN27941 2.925 -0.01 1320 D2163 2.968 0.47				D(0.04)		
1275 EN27941				R(0.01)		
1320 D2163						
1469 1603 3.0316 1.17 1634 ISO7941 3.09 1.82 1677 2.914 -0.13 1776 EN27941 2.955 C 0.33 first reported 1.300 1978 D2163 C005710679 2.9853 0.66 6018 EN27941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6203 EN27941 4.5560 R(0.01) 18.01 6203 EN27941 A.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) R(calc.) Compare R(EN27941:13(liq)) = 0.3886						
1603		D2103				
1634 ISO7941 3.09 1.82 1677 2.914 -0.13 1776 EN27941 2.955 C 0.33 first reported 1.300 1978 D2163 2.7605 -1.82 6016 GOST10679 2.9853 0.66 6018 EN27941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
1677		ISO7941			1.82	
1776 EN27941		1007011				
1978 D2163		EN27941		С		first reported 1,300
6016 GOST10679 2.9853 0.66 6018 EN27941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev. (D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886					-1.82	
6018 EN27941 2.7083 -2.40 6019 ISO7941 2.7509 -1.93 6108 D2163 2.9815 0.62 6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
6019 ISO7941						
6142 6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886	6019		2.7509			
6193 D2163 3.06 1.49 6203 EN27941 4.5560 R(0.01) 18.01 6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886		D2163	2.9815		0.62	
6203 EN27941		_				
6262 D2163 2.8913 -0.38 normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
normality not OK n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886				R(0.01)		
n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev. (D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886	6262	D2163	2.8913		-0.38	
n 40 outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev. (D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886		P.	. 014			
outliers 3 mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886		•				
mean (n) 2.9255 st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886			-			
st.dev. (n) 0.16595 R(calc.) 0.4647 st.dev. (D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
R(calc.) 0.4647 st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
st.dev.(D2163:14) 0.09053 R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886						
R(D2163:14) 0.2535 Compare R(EN27941:13(liq)) = 0.3886		` ,				
x 3.5 Kernel Density						Compare $R(FN27941:13(lig)) = 0.3886$
X Kernel Density			3.2300			
X Kernel Density	42					25
	4./]					~ I I
	4.2					



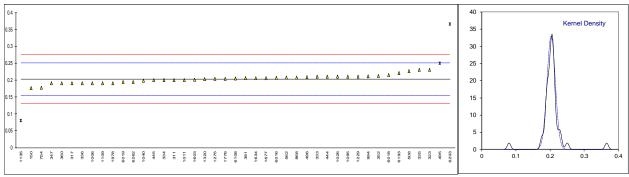
Determination of n-Butane on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	2.459	R(0.05)	-4.57	
171			. ,		
311	D2163	2.82		0.04	
317	D2163	2.85		0.42	
323	D2163	3.10		3.61	
333	D2163	2.86		0.55	
334	D2163	2.83		0.17	
335	D2163	3.04		2.85	
336	D2163	2.70		-1.49	
347	D2163	2.582		-3.00	
352	EN27941	2.9557		1.77	
360	EN27941	2.64		-2.26	
381	DIN51619	2.796		-0.27	
444	IP405	2.939		1.56	
445	D2163	2.80		-0.22	
495	D2163	3.67	R(0.01)	10.89	
496	D2163	2.887	` ,	0.89	
508	D2163	3.204858	R(0.05)	4.95	
529			, ,		
562	D2163	2.865		0.61	
754	D2163	2.575		-3.09	
868	D2163	2.855		0.49	
994	D2163	2.8207		0.05	
1006	D2163	2.677		-1.79	
1011	ISO7941	2.8		-0.22	
1026	ISO7941	2.98	С	2.08	first reported 1.95
1040	DIN51619Mod.	2.744		-0.93	•
1095	ISO7941	2.87		0.68	
1109	IP405	2.41	R(0.05)	-5.20	
1135	D2163	0.97	R(0.01)	-23.58	
1229	IP473	2.82	,	0.04	
1275	EN27941	2.775		-0.54	
1320	D2163	2.816		-0.01	
1469					
1603		2.9908		2.22	
1634	ISO7941	3.035		2.78	
1677		2.778		-0.50	
1776	EN27941	2.819	С	0.03	first reported 0.939
1978	D2163	2.6655	_	-1.93	
6016	GOST10679	2.8743		0.73	
6018	EN27941	2.5347		-3.60	
6019	ISO7941	2.6148		-2.58	
6108	D2163	2.8475		0.39	
6142					
6193	D2163	2.90		1.06	
6203	EN27941	5.9969	R(0.01)	40.60	
6262	D2163	2.7722	(0.01)	-0.57	
				0.01	
	normality	OK			
	n	37			
	outliers	6			
	mean (n)	2.8170			
	st.dev. (n)	0.13203			
	R(calc.)	0.3697			
	st.dev.(D2163:14)	0.07832			
	R(D2163:14)	0.2193			Compare R(EN27941:13(lig)) = 0.3886
	(52100.14)	0.2.00			55ps5 11(E1121011110(119)) = 0.0000



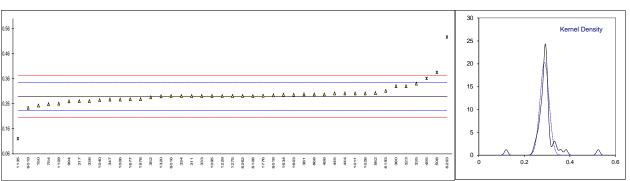
Determination of 1-Butene on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	0.176		-1.13	
171					
311	D2163	0.20		-0.13	
317	D2163	0.19		-0.54	
323	D2163	0.23		1.12	
333	D2163	0.21		0.29	
334	D2163	0.20		-0.13	
335	D2163	0.23		1.12	
336	D2163	0.19		-0.54	
347	D2163	0.19		-0.54	
352	EN27941	0.2122		0.38	
360	EN27941	0.19		-0.54	
381	DIN51619	0.205		0.08	
444	IP405	0.210		0.29	
445	D2163	0.20		-0.13	
495	D2163	0.25	ex	1.96	test result excluded, see §4.1
496	D2163	0.208		0.21	
508	D2163	0.225739		0.95	
529					
562	D2163	0.207		0.17	
754	D2163	0.177		-1.09	
868	D2163	0.207		0.17	
994	D2163	0.2113		0.35	
1006	D2163	0.190		-0.54	
1011	ISO7941	0.2		-0.13	
1026	ISO7941	0.21	С	0.29	first reported 0.15
1040	DIN51619Mod.	0.198		-0.21	
1095	ISO7941	0.21		0.29	
1109	IP405	0.19		-0.54	
1135	D2163	0.08	R(0.01)	-5.13	
1229	IP473	0.21		0.29	
1275	EN27941	0.203		0.00	
1320	D2163	0.202		-0.04	
1469					
1603		0.2008		-0.09	
1634	ISO7941	0.205		0.08	
1677		0.205		0.08	
1776	EN27941	0.203	С	0.00	first reported 0.084
1978	D2163	0.1902		-0.53	
6016	GOST10679	0.2066		0.15	
6018	EN27941	0.2151		0.50	
6019	ISO7941	0.1942		-0.37	
6108	D2163	0.2046		0.07	
6142					
6193	D2163	0.22		0.71	
6203	EN27941	0.3652	R(0.01)	6.76	
6262	D2163	0.1942	` '	-0.37	
	normality	OK			
	n	40			
	outliers	2 (+1 ex)			
	mean (n)	0.2030			
	st.dev. (n)	0.01209			
	R(calc.)	0.0338			
	st.dev.(D2163:14)	0.02398			
	R(D2163:14)	0.0671			Compare R(EN27941:13(liq)) = 0.1610
	, ,				. () () () ()



Determination of iso-Butene on sample #20200; results in %mol/mol

171	lab	method	value	mark	z(targ)	remarks
311 D2163		D2163	0.252		-1.31	
317 D2163 0.27						
323 D2163 0.33 1.47 334 D2163 0.29 0.04 335 D2163 0.29 0.04 336 D2163 0.29 0.04 336 D2163 0.27 -0.67 347 D2163 0.27 -0.67 352 EN27941 0.284 -0.15 360 EN27941 0.33 1.47 381 DIN51619 0.296 0.26 444 IP405 0.300 0.40 445 D2163 0.30 0.40 445 D2163 0.30 0.40 445 D2163 0.30 0.40 445 D2163 0.30 0.40 446 D2163 0.297 0.29 508 D2163 0.327 R(0.01) 3.38 529						
333 D2163 0.29 0.04 334 D2163 0.29 0.04 335 D2163 0.29 0.04 336 D2163 0.34 1.82 336 D2163 0.276 -0.67 347 D2163 0.276 -0.45 347 D2163 0.276 -0.45 352 ENZ7941 0.33 1.47 381 DINS1619 0.296 0.26 4444 IP405 0.300 0.40 4445 D2163 0.30 0.40 4445 D2163 0.36 R(0.05) 2.54 4496 D2163 0.39 0.40 495 D2163 0.383773 R(0.01) 3.38 562 D2163 0.297 0.29 508 D2163 0.257 -1.13 562 D2163 0.257 -1.13 562 D2163 0.257 0.29 568 D2163 0.297 0.29 574 D2163 0.297 0.29 586 D2163 0.297 0.29 587 D2163 0.297 0.29 588 D2163 0.297 0.29 589 D2163 0.297 0.29 599 D2163 0.297 0.29 599 D2163 0.297 0.29 590 D2163 0.297 0.29 591 D2163 0.297 0.29 592 D2163 0.297 0.29 593 D2163 0.297 0.29 594 D2163 0.297 0.29 595 D2163 0.297 0.29 596 D2163 0.297 0.29 597 0.29 598 D2163 0.297 0.29 599 D2163 0.296 0.04 507 D2163 0.297 0.29 508 D2163 0.297 0.29 509 D2163 0.290 0.04 509 D2163 0.290 0.04 509 D2163 0.290 0.04 509 D2163 0.290 0.04 509 D2163 0.299 0.04 509 D2163 0.290		D2163				
334 D2163 0.29 0.04 335 D2163 0.34 1.82 336 D2163 0.27 -0.67 347 D2163 0.27 -0.67 347 D2163 0.27 -0.67 352 EN27941 0.2844 -0.15 360 EN27941 0.33 1.47 381 DIN51619 0.296 0.26 444 IP405 0.300 0.40 445 D2163 0.30 .40 445 D2163 0.36 R(0.05) 2.54 489 D2163 0.397 R(0.01) 3.38 529	323	D2163	0.33		1.47	
336 D2163 0.34 1.82 336 D2163 0.27 - 0.67 347 D2163 0.276 - 0.45 352 ENZ7941 0.33 1.47 360 ENZ7941 0.33 1.47 381 DINS1619 0.296 0.26 4444 IP405 0.300 0.40 4445 D2163 0.30 0.40 4445 D2163 0.30 0.40 4496 D2163 0.297 0.29 508 D2163 0.382773 R(0.01) 3.38 529 0.2163 0.302 0.47 754 D2163 0.257 - 1.13 868 D2163 0.297 0.29 994 D2163 0.2682 0.27 508 D2163 0.297 0.29 994 D2163 0.2682 0.276 1011 ISO7941 0.3 0.40 1011 ISO7941 0.3 0.40 1010 INS1619Mod. 0.274 - 0.52 1010 INS1619Mod. 0.274 - 0.52 1010 INS1619Mod. 0.274 - 0.52 1011 ISO7941 0.9 0.04 1109 IP405 0.26 1.02 11135 D2163 0.289 0.01 11229 IP473 0.29 0.04 1120 D2163 0.288 0.01 1121 ISO7941 0.295 0.025 11263 0.289 0.01 11275 ENZ7941 0.290 0.04 11280 D2163 0.289 0.01 1129 D2163 0.289 0.01 1120 D2163 0.289 0.01 1121 ISO7941 0.295 0.22 1122 IP473 0.290 0.04 1122 IP473 0.000 IP474 0.000 IP474 0.000 IP474 0.000 IP474 0.000 IP474 0.	333	D2163	0.29		0.04	
336 D2163 0.34 1.82 336 D2163 0.27 - 0.67 347 D2163 0.276 - 0.45 352 ENZ7941 0.33 1.47 360 ENZ7941 0.33 1.47 381 DINS1619 0.296 0.26 4444 IP405 0.300 0.40 4445 D2163 0.30 0.40 4445 D2163 0.30 0.40 4496 D2163 0.297 0.29 508 D2163 0.382773 R(0.01) 3.38 529 0.2163 0.302 0.47 754 D2163 0.257 - 1.13 868 D2163 0.297 0.29 994 D2163 0.2682 0.27 508 D2163 0.297 0.29 994 D2163 0.2682 0.276 1011 ISO7941 0.3 0.40 1011 ISO7941 0.3 0.40 1010 INS1619Mod. 0.274 - 0.52 1010 INS1619Mod. 0.274 - 0.52 1010 INS1619Mod. 0.274 - 0.52 1011 ISO7941 0.9 0.04 1109 IP405 0.26 1.02 11135 D2163 0.289 0.01 11229 IP473 0.29 0.04 1120 D2163 0.288 0.01 1121 ISO7941 0.295 0.025 11263 0.289 0.01 11275 ENZ7941 0.290 0.04 11280 D2163 0.289 0.01 1129 D2163 0.289 0.01 1120 D2163 0.289 0.01 1121 ISO7941 0.295 0.22 1122 IP473 0.290 0.04 1122 IP473 0.000 IP474 0.000 IP474 0.000 IP474 0.000 IP474 0.000 IP474 0.	334				0.04	
336 D2163						
347 D2163 0.276 -0.45 352 ENZ7941 0.2844 -0.15 360 ENZ7941 0.33 1.47 381 DIN51619 0.296 0.26 444 IP405 0.300 0.40 445 D2163 0.30 0.40 445 D2163 0.36 R(0.05) 2.54 496 D2163 0.297 0.29 508 D2163 0.297 0.29 508 D2163 0.257 -1.13 529						
352 ENZ7941 0.2844 -0.15 360 ENZ7941 0.33 1.47 381 DIN51619 0.296 0.26 444 IP405 0.30 0.40 445 D2163 0.30 0.40 445 D2163 0.36 R(0.05) 2.54 496 D2163 0.287 0.29 508 D2163 0.383773 R(0.01) 3.38 529						
360 ENZ7941 0.33 1.47 381 DIN51619 0.296 0.26 444 IP405 0.300 0.40 445 D2163 0.30 0.40 496 D2163 0.38 R(0.05) 2.54 496 D2163 0.287 0.29 508 D2163 0.287 0.29 509 D2163 0.257 -1.13 529						
381 DIN51619 0.296 0.26 444 IP405 0.300 0.40 445 D2163 0.30 0.40 4495 D2163 0.39 R(0.05) 2.54 496 D2163 0.297 0.29 508 D2163 0.383773 R(0.01) 3.38 529						
444 P405 0.300 0.40 445 D2163 0.30 0.40 496 D2163 0.26 R(0.05) 2.54 496 D2163 0.29 0.29 508 D2163 0.383773 R(0.01) 3.38 529 562 D2163 0.257 -1.13 568 D2163 0.257 -1.13 569 D2163 0.2682 -0.73 1006 D2163 0.276 -0.45 1011 SO7941 0.3 0.40 1026 SO7941 0.30 C 0.40 1040 D1851619Mod. 0.274 -0.52 1095 SO7941 0.29 0.04 1109 P405 0.26 -1.02 1135 D2163 0.289 0.01 1229 P473 0.29 0.04 1469 1603 D2163 0.289 0.01 1469 1676 ENZ7941 0.290 0.04 1469 1677 0.277 -0.42 1677 0.277 -0.42 1677 D2163 0.2780 0.38 16016 GOST10679 0.2886 0.03 1618 ENZ7941 0.290 0.12 1619 D2163 0.2780 0.38 1618 ENZ7941 0.291 0.42 1619 D2163 0.2780 0.38 1618 ENZ7941 0.292 0.12 1619 D2163 0.2780 0.38 1618 ENZ7941 0.291 0.04 1619 D2163 0.2906 0.07 16142 1619 D2163 0.2906 0.07 16142 1619 D2163 0.31 0.76 16203 ENZ7941 0.5249 R(0.01) 8.40 1620 D2163 0.31 0.76 16203 ENZ7941 0.5249 R(0.01) 8.40 1620 D2163 0.31 0.76 1620 ENZ7941 0.5249 R(0.01) 8.40 1620 D2163 0.2906 0.07 1642 1642 1644 1654 1655 1666 1676 1677 1680 1691 1602 1603 1604						
445 D2163						
496 D2163 0.36 R(0.05) 2.54 496 D2163 0.297 0.29 508 D2163 0.383773 R(0.01) 3.38 529 D2163 0.383773 R(0.01) 3.38 529 D2163 0.257 -1.13 868 D2163 0.287 0.29 994 D2163 0.2682 -0.73 1006 D2163 0.2682 -0.73 1011 ISO7941 0.3 0.40 1026 ISO7941 0.3 0.40 1040 DIN51619Mod. 0.274 -0.52 1095 ISO7941 0.29 0.04 1109 IP405 0.26 -1.02 1135 D2163 0.12 R(0.01) -6.01 1229 IP473 0.29 0.04 1469 -0.2163 0.289 0.01 1677 0.2794 0.295 0.22 1677 0.277 0.04						
996 D2163				D(0.05)		
508 D2163				K(0.05)		
529 562 D2163				D(0.04)		
562 D2163		D2103		K(0.01)		
754 D2163		D0400				
868 D2163						
994 D2163						
1006 D2163						
1011 ISO7941 0.3 0.40 first reported 0.21 1026 ISO7941 0.30 C 0.40 first reported 0.21 1040 DIN51619Mod. 0.274 -0.52 1095 ISO7941 0.29 0.04 1095 ISO7941 0.29 0.04 1109 IP405 0.26 -1.02 1135 D2163 0.12 R(0.01) -6.01 1229 IP473 0.29 0.04 1320 D2163 0.289 0.01 1320 D2163 0.289 0.01 13603 0.2957 0.25 1603 ISO7941 0.295 0.22 1677 0.277 -0.42 1776 EN27941 0.291 C 0.08 first reported 0.122 1978 D2163 0.2780 -0.38 16016 GOST10679 0.2896 0.03 16018 EN27941 0.2922 0.12 16019 ISO7941 0.2434 -1.61 1608 D2163 0.2906 0.07 16142						
1026 ISO7941 0.30 C 0.40 first reported 0.21 1040 DIN51619Mod. 0.274 -0.52 1095 ISO7941 0.29 0.04 1109 IP405 0.26 -1.02 1129 IP473 0.29 0.04 1275 ENZ7941 0.290 0.04 1280 D2163 0.12 R(0.01) -6.01 1290 D2163 0.289 0.01 1469 0.295 0.25 1677 0.297 0.25 1677 0.277 -0.42 1677 0.277 -0.42 1677 0.277 -0.42 1677 0.278 0.38 first reported 0.122 1978 D2163 0.2780 -0.38 6016 GOST10679 0.2896 0.03 6018 ENZ7941 0.292 0.12 6019 ISO7941 0.2934 -1.61 6108 D2163 0.2906 0.07 6142 0.42 6193 D2163 0.31 0.76 6262 D2163 0.31 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 Normality suspect n n 39 outtiers 4 mean (n) 0.2887 st.dev. (D163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		D2163				
1040 DIN51619Mod. 0.274 -0.52 1SO7941 0.29 0.04 1109 IP405 0.26 0.102 1135 D2163 0.12 R(0.01) -6.01 1229 IP473 0.29 0.04 1320 D2163 0.289 0.01 1320 D2163 0.2957 0.25 1634 ISO7941 0.295 0.22 1677 0.277 -0.42 1776 EN27941 0.291 C 0.08 first reported 0.122 1978 D2163 0.2780 -0.38		ISO7941				
1095 ISO7941 0.29 0.04 1109 IP405 0.26 -1.02 1135 D2163 0.12 R(0.01) -6.01 1229 IP473 0.29 0.04 1275 ENZ7941 0.290 0.04 1320 D2163 0.289 0.01 1469	1026	ISO7941	0.30	С	0.40	first reported 0.21
1109	1040	DIN51619Mod.	0.274			
1135 D2163	1095	ISO7941	0.29		0.04	
1135 D2163	1109	IP405	0.26		-1.02	
1229		D2163		R(0.01)		
1275 EN27941 0.290 0.04 1320 D2163 0.289 0.01 1469 1603 0.2957 0.25 1634 ISO7941 0.295 0.22 1776 EN27941 0.291 C 0.08 1978 D2163 0.2780 -0.38 6016 GOST10679 0.2896 0.03 6018 EN27941 0.292 0.12 6019 ISO7941 0.2434 -1.61 6108 D2163 0.2906 0.07 6142 6142 6142 6142 6142 6143 D2163 0.31 0.76 6203 EN27941 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 normality suspect n 39		IP473	0.29	` ,		
1320 D2163			0.290			
1469						
1603						
1634 ISO7941 0.295 0.277 -0.42 1776 EN27941 0.291 C 0.08 first reported 0.122 1778 D2163 0.2780 -0.38 6016 GOST10679 0.2896 0.03 6018 EN27941 0.2922 0.12 6019 ISO7941 0.2434 -1.61 6108 D2163 0.2906 0.07 6142						
1677		ISO7941				
1776 EN27941 0.291 C 0.08 first reported 0.122 1978 D2163 0.2780 -0.38 6016 GOST10679 0.2896 0.03 6018 EN27941 0.2922 0.12 6019 ISO7941 0.2434 -1.61 6108 D2163 0.2906 0.07 6142 6193 D2163 0.31 0.76 6203 EN27941 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 normality suspect n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) st.dev. (D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		1007011				
1978 D2163		EN270/1		$^{\circ}$		first reported 0.122
6016 GOST10679 0.2896 0.03 6018 EN27941 0.2922 0.12 6019 ISO7941 0.2434 -1.61 6108 D2163 0.2906 0.07 6142				C		ilist reported 0.122
6018 EN27941						
6019 ISO7941 0.2434 -1.61 6108 D2163 0.2906 0.07 6142 6193 D2163 0.31 0.76 6203 EN27941 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 normality suspect n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610						
6108 D2163						
6142						
6193 D2163 0.31 0.76 6203 EN27941 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 normality suspect n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		D2103				
6203 EN27941 0.5249 R(0.01) 8.40 6262 D2163 0.2900 0.04 normality suspect n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		D0400				
6262 D2163 0.2900 0.04 normality suspect 0.04 n 39 000 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610				D (0 - :)		
normality suspect n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610				R(0.01)		
n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610	6262	D2163	0.2900		0.04	
n 39 outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		P6				
outliers 4 mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		•				
mean (n) 0.2887 st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610						
st.dev. (n) 0.01964 R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610						
R(calc.) 0.0550 st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610						
st.dev.(D2163:14) 0.02810 R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610						
R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610		R(calc.)	0.0550			
R(D2163:14) 0.0787 Compare R(EN27941:13(liq)) = 0.1610			0.02810			
						Compare R(EN27941:13(liq)) = 0.1610
		` '				
						30



Determination of n-Pentane on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	1.371	R(0.05)	2(tary)	
171	D2100		11(0.00)		
311	D2163	0.94			
317	D2163	0.93			
323	D2163	1.04			
333	D2163	0.95			
334	D2163	0.93			
335	D2163	1.24			
336	D2163	0.88			
347	D2163	0.71			
352	EN27941	1.0030			
360	EN27941	1.14			
381	DIN51619	0.953			
444 445	IP405	0.983			
445	D2163 D2163	0.98 1.56	R(0.05)		
496	D2163	0.983	11(0.00)		
508	D2163	1.368845	R(0.05)		
529	52.00		11(0.00)		
562	D2163	0.970			
754	D2163	0.850			
868	D2163	0.950			
994	D2163	0.9461			
1006	D2163	0.889			
1011	ISO7941	1.0			
1026	ISO7941	1.00	С		first reported 0.43
1040	DIN51619Mod.	0.860			
1095	ISO7941	0.96			
1109	IP405	0.63	D (2.24)		
1135	D2163	0.12	R(0.01)		
1229	IP473	0.95			
1275	EN27941	0.909			
1320 1469	D2163	0.942			
1603		0.9849			
1634	ISO7941	1.185			
1677	1007541	0.917			
1776	EN27941	0.934	С		first reported 0.106
1978	D2163	0.8076	Ü		mot reported 6.100
6016	GOST10679	0.9606			
6018	EN27941	0.7893			
6019	ISO7941	1.6218	R(0.05)		
6108	D2163	0.9422	, ,		
6142					
6193	D2163	0.96			
6203	EN27941	3.3155	R(0.01)		
6262	D2163	0.7375			
	normality	not OV			
	normality n	not OK 37			
	outliers	6			
	mean (n)	0.9388			
	st.dev. (n)	0.11472			
	R(calc.)	0.3212			
	st.dev.(D2163:14)	(0.03239)			
	R(D2163:14)	(0.0907)			Compare R(EN27941:13(liq)) = 0.3131
2 T					6
1.8 -					Kernel Density
1.6					x x 5]
1.4 -					x x 4
1.2 -					
1		<u> </u>	<u> </u>	<u>, </u>	<u>A A A A A</u> 3
0.8	Δ Δ Δ " "				
0.6					
0.4 -					1 - //
0.2 + x					
1136	3262 3018 1978 1978 1040 1006 1275 1677	317 320 3108 333	38.1 38.1 38.1	86 4 4 8 8 8 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
	~~	~ + 0	0	,	

Determination of iso-Pentane on sample #20200; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
150	D2163	<0.01			
171					
311					
317	D2163	<0.01			
323	D2163	< 0.01			
333	D2163	< 0.01			
334	D2163	< 0.01			
335	D2163	< 0.01			
336	D2163	<0.01			
347					
352					
360	EN27941	< 0.1			
381	DIN51619	0.034			as per DIN51619 result is <0.1
444	IP405	0.003			rounded result is <0.1
445	D2163	<0.01			
495	D2163	<0,01			recorded resolution 0.04
496	D2163	0.003			rounded result is <0.01
508	D2163	0.000000			
529					
562					
754	D2162	0.003			
868 994	D2163 D2163	<0.01			
1006	D2163	0			
1011	ISO7941	< 0.1			
1026	ISO7941	0.00			
1040	DIN51619Mod.	0.003			
1095	ISO7941	0.00			rounded result <0.1
1109	IP405	0.00			
1135	D2163	<0.01			
1229	IP473	0			
1275	EN27941	0.003			
1320					
1469					
1603					
1634	ISO7941	0.00			
1677		0.003			rounded result <0.01
1776					
1978					
6016					
6018					
6019					
6108	D2163	<0.01			
6142	D0100				
6193	D2163	0			
6203	EN27941	0.0241			
6262	D2163	<0.01			
	_	07			
	n maan (n)	27			
	mean (n)	<0.01			

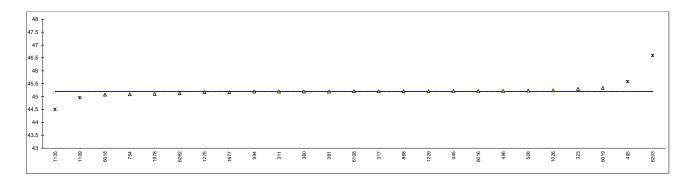
Total of reported composition (normalized) test results; results in %mol/mol

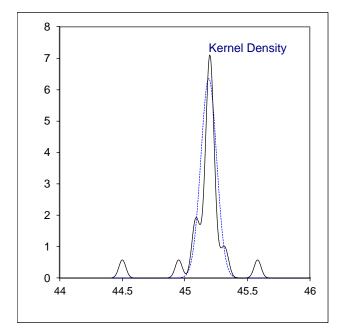
lab	method	value	remarks
150	D2163	100.00	
171			
311	D2163	99.99	
317	D2163	100.00	
323	D2163	99.98	
333	D2163	100.00	
334	D2163	100.00	
335 336	D2163 D2163	100.00 100.01	
347	D2163 D2163	100.01	
352	EN27941	100.00	
360	EN27941	100.00	
381	DIN51619	100.00	
444	IP405	100.00	
445	D2163	100.00	
495	D2163	100.00	
496	D2163	100.00	
508	D2163	100.00	
529			
562	D2163	100.00	
754	D2163	100.00	
868	D2163	100.00	
994	D2163	99.98	
1006	D2163	100.00	
1011	ISO7941	100.80	Not 100%
1026	ISO7941	100.00	
1040	DIN51619Mod.	100.19	
1095	ISO7941	100.00	
1109 1135	IP405	100.00 99.99	
	D2163		
1229 1275	IP473 EN27941	100.01 100.00	
1320	D2163	100.00	
1469	D2 103		
1603		100.00	
1634	ISO7941	100.00	
1677		100.00	
1776	EN27941	100.00	
1978	D2163	100.04	
6016	GOST10679	100.00	
6018	EN27941	99.99	
6019	ISO7941	99.99	
6108	D2163	100.00	
6142	D 0100		
6193	D2163	99.52	Not 100%
6203	EN27941	100.00	
6262	D2163	100.00	

Determination of Molar Mass on sample #20200; results in g/mol

lab	method	value	mark z	z(targ)	remarks
150					
171					
311	D2598	45.19			
317	INH-001	45.2			
323	D2598	45.30			
333					
334					
335					
336					
347					
352					
360	ISO8973	45.19			
381	ISO8973	45.1943			
444	D0400	45.000			
445	D2163	45.209			test result and old as CAA
495	D2163	45.58 45.346	ex		test result excluded, see §4.1
496	D2163	45.216	_		coloulation difference, iie coloulate - 1 45 4444
508	D2598	45.228119	E		calculation difference, iis calculated 45.444
529 563					
562 754	D2421	45.085			
754 868	D2598	45.065 45.20			
994	D2596 D2163	45.20 45.1845			
1006	DZ 100	45.1645			
1011					
1026	ISO8973	45.24	С		first reported 44.80
1040	.500010		•		
1095					
1109	ISO8973	44.950	R(0.05)		
1135	D2598	44.5	ex		test result excluded, see §4.1
1229	ISO8973	45.20			, ,
1275	EN589	45.166	С		first reported 45.137
1320					•
1469					
1603					
1634					
1677	D2163	45.169			
1776					
1978	D2598	45.0903			
6016	1000070	45.21			
6018	ISO8973	45.07			
6019	ISO8973	45.33			
6108	D2163	45.1987			
6142					
6193	ISO9073	46 5021	OV		tost result evaluded, see 84.1
6203	ISO8973 D2163	46.5921 45.12	ex		test result excluded, see §4.1
6262	DZ103	40.12			
					iis calc. based on ALL reported composition results: *)
	normality	ОК			OK
	n	21			36
	outliers	1 (+3 ex)			2 (+5 ex)
	mean (n)	45.190			45.193
	st.dev. (n)	0.0628	RSD = 0.14%	6	0.0609 RSD = 0.13%
	R(calc.)	0.176	,		0.170
	compare				
	R(iis19S03P)	0.083			0.072
	R(iis18S03P)	0.098			0.173

^{*)} Calculated by iis based on relative molecular masses as given in table 2 of ASTM D2421:19 NB. Effect of different factors of ASTM D2421:19 and ISO8973:97/IP432:00(2017) on the calculation is very small

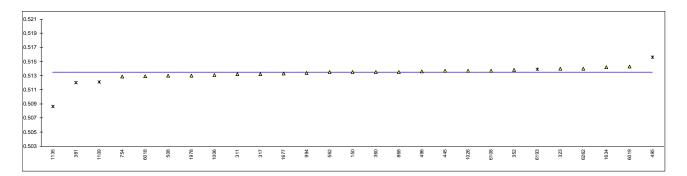


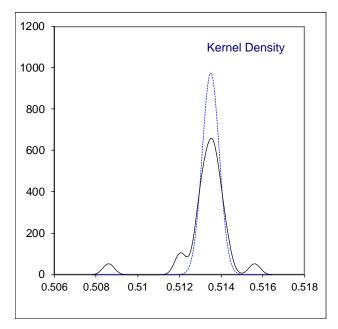


Determination of Relative Density at 60/60°F on sample #20200;

lab	method	value	mark	z(targ)	remarks
150	D2598	0.5135		<u></u>	
171	D2330				
311	D2598	0.5132			
317	INH-001	0.5132			
323	D2598	0.514			
333					
334					
335					
336					
347					
352	ISO8973	0.5138			
360	D2598	0.5135			
381	D2598	0.512	DG(0.05)		
444			, ,		
445	ISO8973	0.5137			
495	D2598	0.5156	ex		test result excluded, see §4.1
496	D2598	0.51359			
508	D2598	0.513			
529					
562	D2598	0.5135			
754	D2598	0.51285			
868	D2598	0.5135			
994	D2598	0.5134			
1006	D2598	0.5131			
1011					
1026	ISO8973	0.5137	С		first reported 0.5112
1040					
1095					
1109	D2598	0.5121	DG(0.05)		
1135	D2598	0.5086	ex		test result excluded, see §4.1
1229					
1275					
1320					
1469					
1603	1000070	0.5440			
1634	ISO8973	0.5142			
1677	D2598	0.51331			
1776	Doron	0.5400			
1978	D2598	0.5130			manustral 4 F000 as Balatina Basaita at 0000
6016	1000070	0.5400			reported 1.5603 as Relative Density at 20°C
6018	ISO8973	0.5129			
6019	ISO8973	0.5143			
6108	D2598	0.5137 			
6142	1509073		OV		test result excluded, see §4.1
6193	ISO8973	0.5139	ex		test result excluded, see 94.1
6203 6262	D2508	0.5140			
0202	D2598	0.5140			
					iis calc, based on ALL reported composition results: *)
	normality	OK			OK
	n	22			36
	outliers	2 (+3 ex)			2 (+5 ex)
	mean (n)	0.51350			0.51344
	st.dev. (n)	0.000409	RSD = 0.08%		0.000366 RSD = 0.07%
	R(calc.)	0.000403	.102 = 0.0070		0.00102
	compare	0.00110			5.00.0 <u>-</u>
	R(iis19S03P)	0.00039			0.00042
	R(iis18S03P)	0.00129			0.00081
	(/				

^{*)} Calculated by iis based on relative densities at 60°F (15.6°C) as given in table 1 of ASTM D2598:16 N.B. Effect of different factors from ASTM D2598:16 and ISO8973:97/IP432:00(2017) on the calculation is very small.





Determination of Absolute Vapor Pressure at 100°F on sample #20200; results in psi

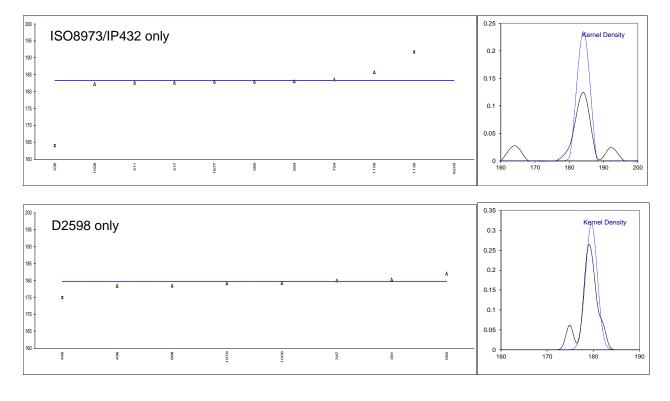
lab	method	ISO8973	mark	z(targ)	D2598	mark	z(targ)	remarks
150								
171								
311	ISO8973	182.6						
317	ISO8973	182.6						
323	1000070							
333								
334	1000072	164.0	F C(0.04)					cala difforance iia cala 100.00
335	ISO8973	164.0	E, G(0.01)					calc. difference, iis calc. 180.82
336	Docoo				400			
347	D2598				180			
352								
360	ISO8973	182.9				_		
381	D2598				180.28	E		calc. difference, iis calc. 178.60
444								
445								
495	D2598				174.9	ex		test result excluded, see §4.1
496	D2598				178.35			
508								
529								
562	D2598				182	E		calc. difference, iis calc. 178.44
754	ISO8973	183.53						,
868	D2598				178.5			
994	ISO8973	182.97						
1006	D2598				179.2			
1011	D2000							
1026	ISO8973	182.2	С					first reported 186.1
1040	1000070		· ·					mot reported 100.1
1095								
11093	ISO8973	185.73						
1135	ISO8973		04					toot rocult avaluded, and \$4.1
	1300973	191.6	ex					test result excluded, see §4.1
1229								
1275								
1320								
1469								
1603								
1634								
1677	ISO8973	182.854						
1776								
1978	D2598				179.1200			
6016								
6018								
6019								
6108								
6142								
6193								
6203	ISO8973	1180.420	U, ex					see remark below this table
6262			, -					
					1			

Lab 6203: test result excluded, see §4.1, U = possibly reported in kPa

	ISO8973/IP432	D2598				
normality n outliers mean (n) st.dev. (n) R(calc.) compare R(iis19S03P) R(iis18S03P)	not OK 8 1 (+2 ex) 183.173 1.1011 RSD = 0.6% 3.083	unknown 7 0 (+1 ex) 179.636 1.2607 RSD = 0.7% 3.530 0.801 2.239				
	iis calc. based on ALL *) reported composition results	iis calc. based on ALL **) reported composition results				
normality n outliers mean (n) st.dev. (n) R(calc.) compare R(iis19S03P) R(iis18S03P)	OK 35 3 (+5 ex) 182.725 0.4998 RSD = 0.3% 1.399 0.967 0.872	suspect 36 2 (+5 ex) 178.598 0.6194 RSD = 0.3% 1.734 0.964 1.007				

- *) Calculated by iis based on Vapor Pressure factors at 100°F (37.8°C) as given in table A.1 of ISO8973:97/IP432:00(2017)

 **) Calculated by iis based on Vapor Pressure factors at 100°F (37.8°C) as given in table 1 of ASTM D2598:16.



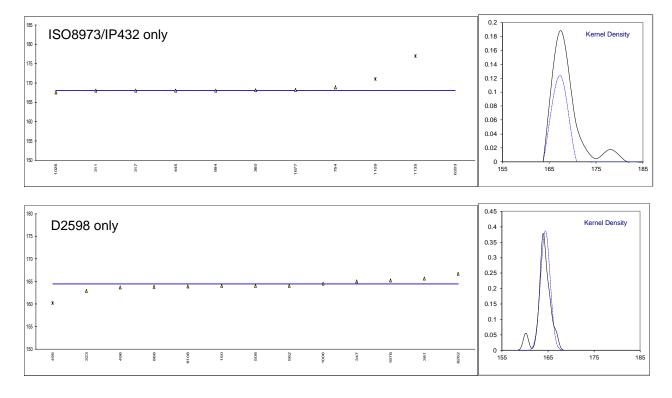
Determination of Relative Vapor Pressure at 100°F on sample #20200; results in psi

lab	method	ISO8973	mark	z(targ)	D2598	mark	z(targ)	remarks
150	D2598				164.0			
171								
311	ISO8973	168						
317	ISO8973	168.0						
323	D2598				162.88			
333								
334								
335								
336	D2509				165			
347 352	D2598				165			
360	ISO8973	168.1						
381	D2598				165.58	Е		calc. difference, iis calc. 163.91
444	D2390					_		calc. difference, its calc. 103.91
445	ISO8973	168						
495	D2598				160.2	ex		test result excluded, see §4.1
496	D2598				163.65	•		toot rooms enoladou, eee 3
508	D2598				164	E		calc. difference, iis calc. 161.58
529								,
562	D2598				164			
754	ISO8973	168.84						
868	D2598				163.8			
994	ISO8973	168.02						
1006	D2598				164.5			
1011			_					
1026	ISO8973	167.5	С					first reported 171.4
1040								
1095	1000070	474.04	D(0.05)					
1109	ISO8973	171.04	D(0.05)					toot requit evaluded and \$4.1
1135 1229	ISO8973	176.9 	ex					test result excluded, see §4.1
1229								
1320								
1469								
1603								
1634								
1677	ISO8973	168.158						
1776								
1978	D2598				165.1979			
6016								
6018								
6019								
6108	D2598				163.8234			
6142								
6193								
6203	ISO8973	1079	U, ex			_		see remark below this table
6262	D2598				166.7	E		calc. difference, iis calc. 164.47

Lab 6203: test result excluded, see §4.1, U = possibly reported in kPa

	ISO8973/IP432	D2598			
normality n outliers mean (n) st.dev. (n) R(calc.) compare R(iis19S03P) R(iis18S03P)	not OK 8 1 (+2 ex) 168.077 0.3671 RSD = 0.2% 1.028	OK 12 1 (+1 ex) 164.428 1.0324 RSD = 0.6% 2.891			
	iis calc. based on ALL *) reported composition results	iis calc. based on ALL **) reported composition results			
normality n outliers mean (n) st.dev. (n) R(calc.) compare	OK 35 3 (+5 ex) 168.029 0.4998 RSD = 0.3% 1.399	suspect 36 2 (+5 ex) 163.902 0.6194 RSD = 0.4% 1.734			

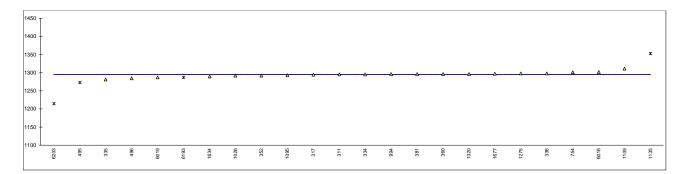
- *) Calculated by iis based on Vapor Pressure factors at 100°F (37.8°C) as given in table A.1 of ISO8973:97/IP432:00(2017)
 **) Calculated by iis based on Vapor Pressure factors at 100°F (37.8°C) as given in table 1 of ASTM D2598:16.

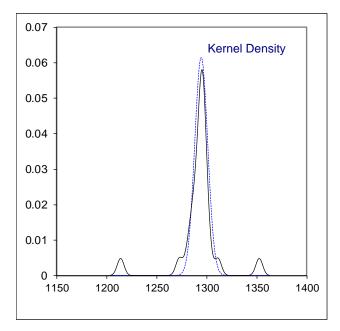


Determination of Absolute Vapor Pressure at 40°C on sample #20200; results in kPa

lab	method	value	mark z	z(targ)	remarks
150					
171					
311	ISO8973	1295			
317	ISO8973	1294			
323					
333					
334	ISO8973	1295			
335	ISO8973	1281			
336	ISO8973	1298			
347					
352	ISO8973	1292			
360	ISO8973	1296			
381	ISO8973	1296			
444					
445					
495	ISO8973	1272.7	ex		test result excluded, see §4.1
496	ISO8973	1284.23	E		calculation difference, iis calculated 1293.32
508					
529					
562					
754	ISO8973	1300.58			
868	100000				
994	ISO8973	1295.84			
1006					
1011	1000070	4004.0	•		" · · · · · · · · · · · · · · · · · · ·
1026	ISO8973	1291.6	С		first reported 1318.3
1040	1000070	4000			
1095	ISO8973	1293			
1109	ISO8973	1311.37	0 1/		took required and background and the
1135	ISO8973	1352.6	ex		test result excluded, see §4.1
1229 1275	EN589	1297.5	С		first reported 1365.7
1320	ISO8973	1297.5	C		ilist reported 1303.7
1469	1300973	1290			
1603					
1634	ISO8973	1289.325			
1677	ISO8973	1296.8			
1776	1000070				
1978					
6016					
6018	ISO8973	1302			
6019	ISO8973	1287			
6108					
6142					
6193	ISO8973	1287	ex		test result excluded, see §4.1
6203	ISO8973	1214.048	ex		test result excluded, see §4.1
6262					3
					iis calc. based on ALL reported composition results: *)
	normality	suspect			OK
	n	20			35
	outliers	0 (+4 ex)			3 (+5 ex)
	mean (n)	1294.612			1294.962
	st.dev. (n)	6.4932	RSD = 0.5%		3.5202 RSD = 0.3%
	R(calc.)	18.181			9.857
	compare				
	R(iis19S03P))	4.81			6.89
	R(iis18S03P)	8.61			10.39

^{*)} Calculated by iis based on the Vapor Pressure factors at 40°C as given in table A.1 of ISO8973:97/IP432:00(2017)



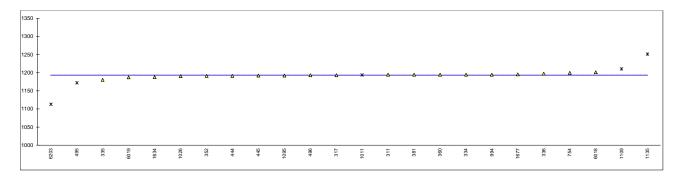


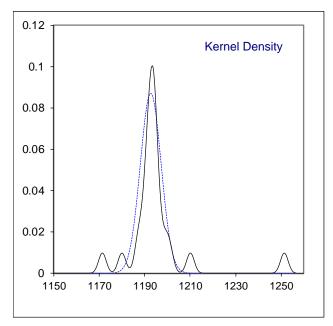
Determination of Relative Vapor Pressure at 40°C on sample #20200; results in kPa

lab	method	value	mark	z(targ)	remarks
150					
171					
311	ISO8973	1194			
317 323	ISO8973	1193 			
333					
334	ISO8973	1194			
335	ISO8973	1180			
336	ISO8973	1197			
347					
352	ISO8973	1191			
360	ISO8973	1194			
381 444	ISO8973 ISO8973	1194 1191.2			
445	ISO8973	1191.5			
495	ISO8973	1171.4	ex		test result excluded, see §4.1
496	ISO8973	1192.90			· · · · · · · · · · · · · · · · · · ·
508					
529					
562	1000070	4400.05			
754	ISO8973	1199.25			
868 994	ISO8973	 1194.54			
1006	1000973				
1011	ISO8973	1193.7	E, ex		see remark below this table
1026	ISO8973	1190.3	C		first reported 1217.0
1040					
1095	ISO8973	1192			
1109	ISO8973	1210.07	G(0.05)		test mesself such ada di see CAA
1135	ISO8973	1251.3	ex		test result excluded, see §4.1
1229 1275					
1320					
1469					
1603					
1634	ISO8973	1188			
1677	ISO8973	1195.5			
1776					
1978					
6016 6018	ISO8973	1201			
6019	ISO8973	1187			
6108					
6142					
6193					
6203	ISO8973	1113	ex		test result excluded, see §4.1
6262					
					iis calc. based on ALL reported composition results: *)
	normality	not OK			OK
	n	19			35
	outliers	1 (+4 ex)			3 (+5 ex)
	mean (n)	1192.642			1193.637
	st.dev. (n)	4.5767	DOD	,	3.5202
	R(calc.)	12.815	RSD = 0.4%	ó	9.857 RSD = 0.3%
	compare R(iis19S03P))	5.44			6.89
	R(iis18S03P)	10.79			10.39
					. 5.55

Lab 1011: test result excluded, see §4.1, calculation difference, iis calculated 1204.56

^{*)} Calculated by iis based on the Vapor Pressure factors at 40°C as given in table A.1 of ISO8973:97/IP432:00(2017)





Determination of Motor Octane Number, MON on sample #20200;

lab	method	EN589	mark	z(targ)	D2598	mark	z(targ)	remarks
150								
171								
311								
317	EN589	95.0						
323								
333								
334	EN589	95.0						
335								
336	EN589	95.0						
347								
352								
360	EN589	95.0						
381	EN589	95.0						
444								
445								
495	EN589	95.0	ex					test result excluded, see §4.1
496	D2598				96.262			,
508	D2598				96.5	Е		see remark below this table
529								
562	D2598				96.0			
754	EN589	95.06						
868	D2598				96.4			
994	EN589	95.03						
1006								
1011								
1026	EN589	95.00	С					first reported 95.12
1040								
1095								
1109	EN589	95.0						
1135	D2598				94.3	E, ex		see remark below this table
1229								
1275	EN589	95.0	С					first reported 94.8
1320	EN589	95.4	E					see remark below this table
1469								
1603								
1634								
1677	EN589	95.55	E, G(0.05)					see remark below this table
1776								
1978	D2598				95.0483	E, G(0.05)		see remark below this table
6016								
6018	EN589	94.1	E, G(0.01)					see remark below this table
6019	EN589	93.5	E, G(0.05)					see remark below this table
6108	D2598				96.0357	E		see remark below this table
6142								
6193	EN589	94.553	ex					test result excluded, see §4.1
6203	EN589	94.6	ex					test result excluded, see §4.1
6262								

Lab 508: calculation difference, iis calculated with D2598 96.07 Lab 1135: test result excluded, see §4.1, calculation difference, iis calculated with D2598 96.85

Lab 1320: calculation difference, iis calculated with EN589 95.02

Lab 1677: calculation difference, iis calculated with EN589 95.04
Lab 1978: calculation difference, iis calculated with D2598 96.37 and with EN589 95.08

Lab 6018: calculation difference, iis calculated with EN589 95.04

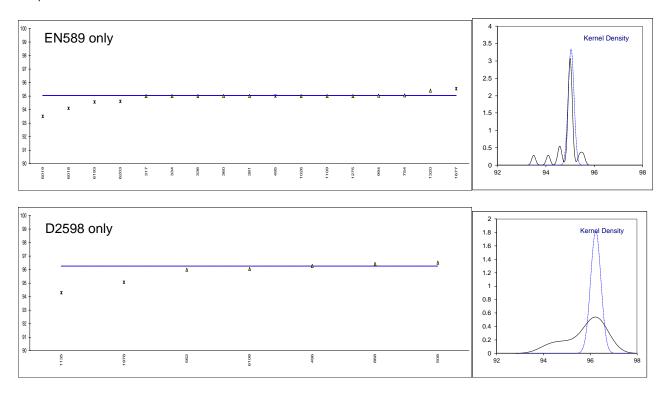
Lab 6019: calculation difference, iis calculated with EN589 95.02

Lab 6108: calculation difference, iis calculated with D2598 96.29

	EN589	D2598				
normality n outliers mean (n) st.dev. (n) R(calc.) compare R(iis19S03P) R(iis18S03P)	not OK 11 3 (+3 ex) 95.045 0.1194 RSD = 0.1% 0.334	unknown 5 1 (+1 ex) 96.240 (0.2197) (RSD = 0.2%) (0.615) (1.003) (1.229)				
	iis calc. based on ALL *) reported composition results	iis calc. based on ALL **) reported composition results				
normality n outliers mean (n) st.dev. (n) R(calc.) compare R(iis19S03P) R(iis18S03P)	suspect 37 1 (+5 ex) 95.024 0.0237 RSD = 0.02% 0.066 0.050 0.049	suspect 38 0 (+5 ex) 96.285 0.0869 RSD = 0.09% 0.243 0.057 0.064				

^{*)} Calculated by iis based on MON factors given in table B.1 of EN589:18.

**) Calculated by iis based on MON factors given in table 1 of ASTM D2598:16. This method does not mention MON factors for iso-Butene. For iso-Butene the value of 83.5 of cis-2-Butene is used in the calculations in analogy of the MON factors of the other components.

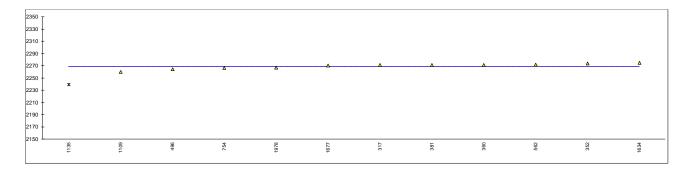


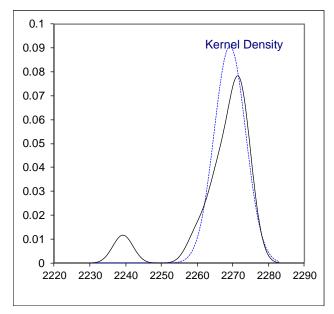
Determination of Ideal Gross Heating Value at 14.696 psia and 60°F on sample #20200; results in kJ/mol

ICGUITG	III KO/IIIOI		<u> </u>		
lab	method	value	mark z	(targ)	remarks
150					
171					
311					
317	D3588	2271.08			
323					
333					
334					
335					
336					
347					
352	D3588	2273.5623			
360	D3588	2271.47			
381	D3588	2271.35			
	D3300				
444					
445					
495					
496	D3588	2264.36	E		calculation difference, iis calculated 2272.38
508	20000		_		
529					
562	D3588	2271.9			
754	D3588	2266.38			
868					
994					
1006					
1011					
1026					
1040					
1095					
	D2500				
1109	D3588	2259.90	_		
1135	D3588	2239.3	E, ex		see remark below this table
1229					
1275					
1320					
1469					
1603					
1634	D3588	2274.55			
1677	D3588	2270.24			
1776					
1978	D3588	2266.6108			
	D3300				
6016					reported 96.28 as IGHV at 14.696 psia and 20°C
6018					
6019					
6108					
6142					
6193					
6203					
6262					
					iis calc. based on ALL reported composition results: *)
	normality	OK			OK
	•	11			36
	n				
	outliers	0 (+1 ex)			2 (+5 ex)
	mean (n)	2269.219			2271.362
	st.dev. (n)	4.4034	RSD = 0.2 %		2.8490 RSD = 0.1%
	R(calc.)	12.330			7.977
		12.000			1.011
	compare	0.00			0.05
	R(iis19S03P))	3.30			3.35
	R(iis18S03P)	11.72			8.13
	•				

Lab 1135: test result excluded, see §4.1, calculation difference, iis calculated 2232.89

^{*)} Calculated by iis based on the Ideal Gross Heating Value at 14.696 psia/60°F factors given in table 1 of ASTM D3588:98(2017).



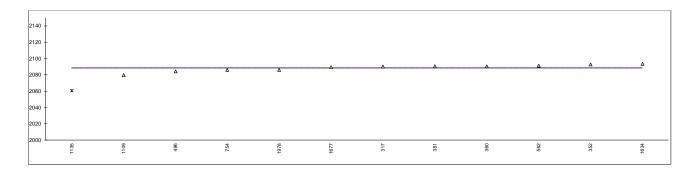


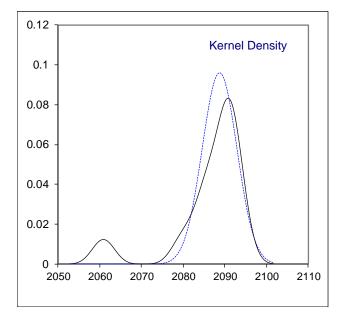
Determination of Ideal Net Heating Value at 14.696 psia and 60°F on sample #20200; results in kJ/mol

	in KJ/moi	•	 	4	
lab	method	value	mark :	z(targ)	remarks
150					
171					
311					
317	D3588	2090.40			
323					
333					
334					
335					
336					
347					
352	D3588	2092.6669			
360	D3588	2090.76			
381	D3588	2090.67			
444					
445					
495					
496	D3588	2084.14	Е		calculation difference, iis calculated 2091.64
508			_		
529					
562	D3588	2091.3			
754	D3588	2085.99			
868					
994					
1006					
1011					
1026					
1040					
1095					
1109	D3588	2079.77			
1135	D3588	2060.8	E, ex		see remark below this table
1229			•		
1275					
1320					
1469					
1603					
	D2500				
1634	D3588	2093.66			
1677	D3588	2089.61			
1776					
1978	D3588	2086.2101			
6016					reported 88.62 as INHV at 14.696 psia and 20°C
6018					
6019					
6108					
6142					
6193					
6203					
6262					
					iis calc. based on ALL reported composition results: *)
	normality	OK			OK
	n	11			36
	outliers	0 (+1 ex)			2 (+5 ex)
	mean (n)	2088.653	DCD 000		2090.679
	st.dev. (n)	4.1593	RSD = 0.2 %)	2.6574 RSD = 0.1%
	R(calc.)	11.646			7.441
	compare				
	R(iis19S03P))	3.16			3.14
	R(iis18S03P)	11.04			7.59

Lab 1135: test result excluded, see §4.1, calculation difference, iis calculated 2054.79

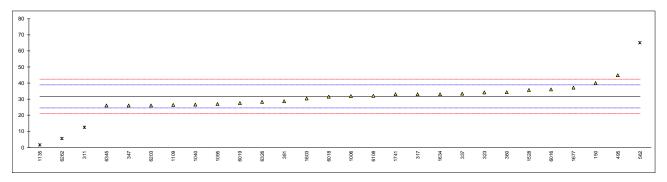
^{*)} Calculated by iis based on the Ideal Net Heating Value at 14.696 psia/60°F factors given in table 1 of ASTM D3588:98(2017).

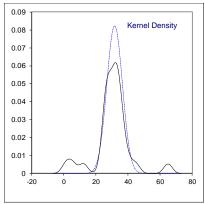




Determination of Total Sulfur on sample #20201; results in mg/kg

lah	mothod	volue	mork	7/tore\	romarka
lab 150	method D6667	value 40.0	mark C	z(targ) 2.32	remarks first reported 5.3
171	D0001	40.0	C	2.32	ilist reported 5.5
311	D6667	12.4	C,R(0.05)	-5.45	first reported 6.4
317	D6667	33	0,11(0.00)	0.35	mot roportou o. r
323	D6667	34		0.63	
337	D6667	33.4	С	0.46	first reported 6.7
347	D6667	26	•	-1.62	
360	D6667	34.3		0.72	
381	D6667	28.7		-0.86	
445					
495	D6667	44.9		3.70	
562	D6667	65	R(0.05)	9.36	
754			,		
1006	D6667	31.8		0.01	
1011					
1040	ISO20846	26.5		-1.48	
1095	D6667	27		-1.34	
1109	D6667	26.38		-1.52	
1135	D6667	1.5	R(0.05)	-8.52	
1528	D6667	35.66	C	1.10	first reported 45.66
1603		30.4		-0.38	
1634	D6667	33		0.35	
1677	D6667	37.04		1.49	
1741	D6667	32.9		0.32	
6016	D6667	36.02		1.20	
6018	D6667	31.37		-0.11	
6019	D6667	27.59		-1.17	
6108	D6667	31.995		0.07	
6142					
6203	D6667	26.06		-1.61	
6262	D6667	5.506	R(0.05)	-7.39	
6326	D6667	28.326		-0.97	
6345	D6667	25.93		-1.64	
	normality	OK			
	n	24			
	outliers	4			
	mean (n)	31.761			
	st.dev. (n)	4.8448			
	R(calc.)	13.565			
	st.dev.(D6667:14)	3.5505			
	R(D6667:14)	9.941			
	, ,				





APPENDIX 2

Number of participants per country

Liquified Propane iis20S03P

1 lab in AUSTRALIA 1 lab in AZERBAIJAN

3 labs in BELGIUM

1 lab in BULGARIA

2 labs in CHILE

1 lab in CHINA, People's Republic

1 lab in DENMARK

1 lab in EGYPT

1 lab in ESTONIA

1 lab in FINLAND

4 labs in FRANCE

4 labs in GERMANY

1 lab in IRELAND

1 lab in KAZAKHSTAN

1 lab in MEXICO

3 labs in NETHERLANDS

1 lab in PANAMA

6 labs in PORTUGAL

1 lab in ROMANIA

1 lab in RUSSIAN FEDERATION

1 lab in SERBIA

1 lab in SLOVAKIA

1 lab in SPAIN

1 lab in SWEDEN

1 lab in TAIWAN

3 labs in UNITED KINGDOM

2 labs in UNITED STATES OF AMERICA

1 lab in VIETNAM

Sulfur (total) in LPG iis20S03S

1 lab in AUSTRALIA

3 labs in BELGIUM

1 lab in BULGARIA

1 lab in CHILE

1 lab in ESTONIA

1 lab in FRANCE

3 labs in GERMANY

1 lab in IRELAND

1 lab in KAZAKHSTAN

1 lab in MALAYSIA

2 labs in NETHERLANDS

5 labs in PORTUGAL

2 labs in ROMANIA

1 lab in RUSSIAN FEDERATION

2 labs in SERBIA

1 lab in SPAIN

1 lab in TAIWAN

1 lab in UNITED KINGDOM

3 labs in UNITED STATES OF AMERICA

1 lab in VIETNAM

APPENDIX 3

Abbreviations

C = final result after checking of first reported suspect test result

 $\begin{array}{ll} D(0.01) &= \text{outlier in Dixon's outlier test} \\ D(0.05) &= \text{straggler in Dixon's outlier test} \\ G(0.01) &= \text{outlier in Grubbs' outlier test} \\ G(0.05) &= \text{straggler in Grubbs' outlier test} \\ DG(0.01) &= \text{outlier in Double Grubbs' outlier test} \\ DG(0.05) &= \text{straggler in Double Grubbs' outlier test} \\ \end{array}$

R(0.01) = outlier in Rosner's outlier test R(0.05) = straggler in Rosner's outlier test

E = calculation difference between reported result and result calculated by iis

ex = test result excluded from the statistical evaluation

n.a. = not applicable
n.d. = not detected
n.e. = not evaluated
fr. = first reported
SDS = safety data sheet

Literature

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- 3 ISO5725, parts 1-6:94
- 4 ISO13528:05
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- 6 W.J. Youden and E.H. Steiner, Statistical Manual of the AOAC, (1975)
- 7 IP367:15
- 8 DIN38402 T41/42
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- 10 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
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- Bernard Rosner, Percentage Points for a Generalized ESD Many-Outlier Procedure, Technometrics, 25(2), 165-172, (1983)
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